



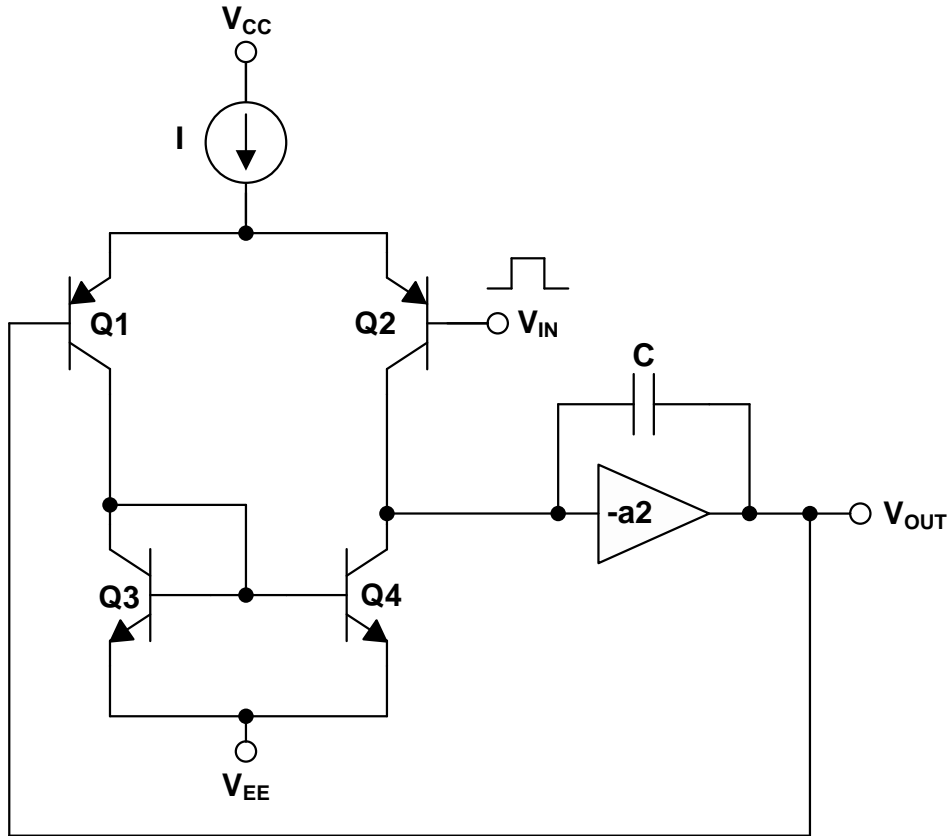
# Current-Feedback Amplifiers – Part 2

TIPL 2012

TI Precision Labs: High-Speed Operational Amplifiers

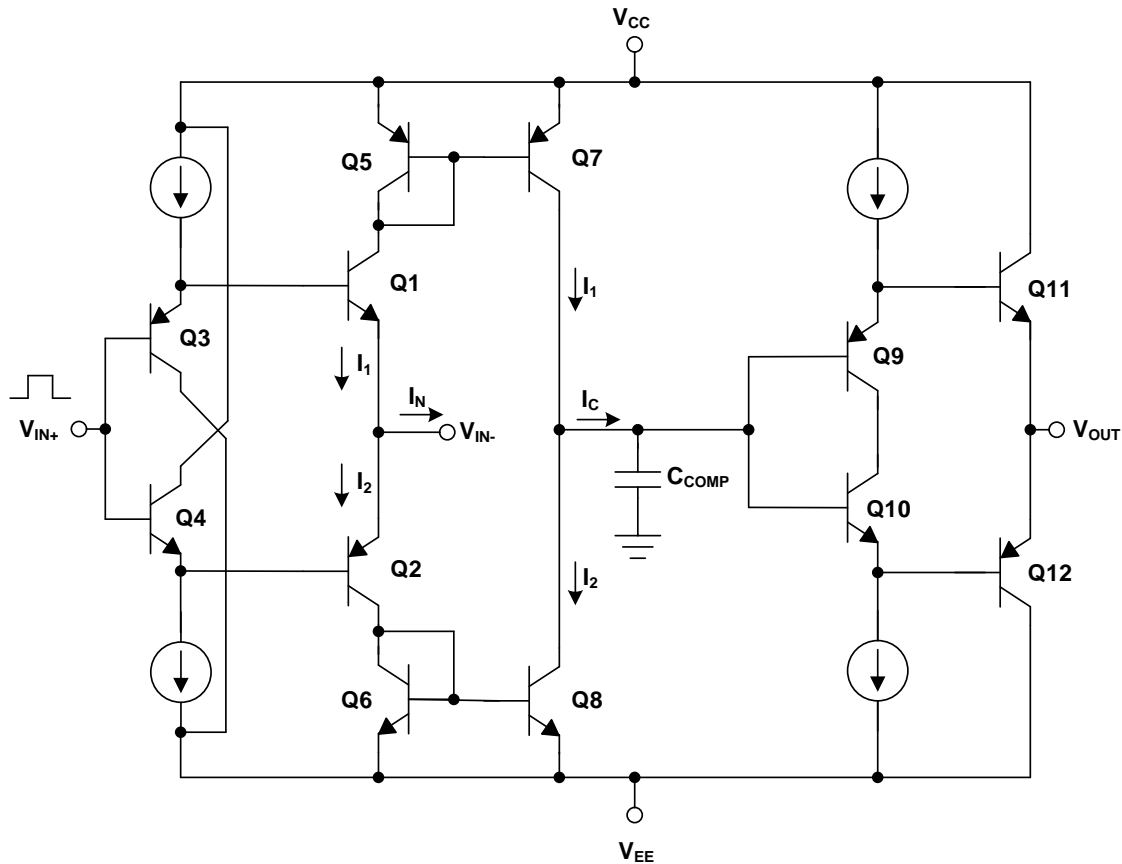
Prepared and Presented by Samir Cherian

# Slew-rate Limitation of VFB



- If  $I = 100\mu\text{A}$  and  $C = 10\text{pF}$ , then,  
Slew Rate =  $100\mu\text{A}/10\text{pF} = 10\text{V} / \mu\text{s}$

# Slew Rate Enhancement with CFB

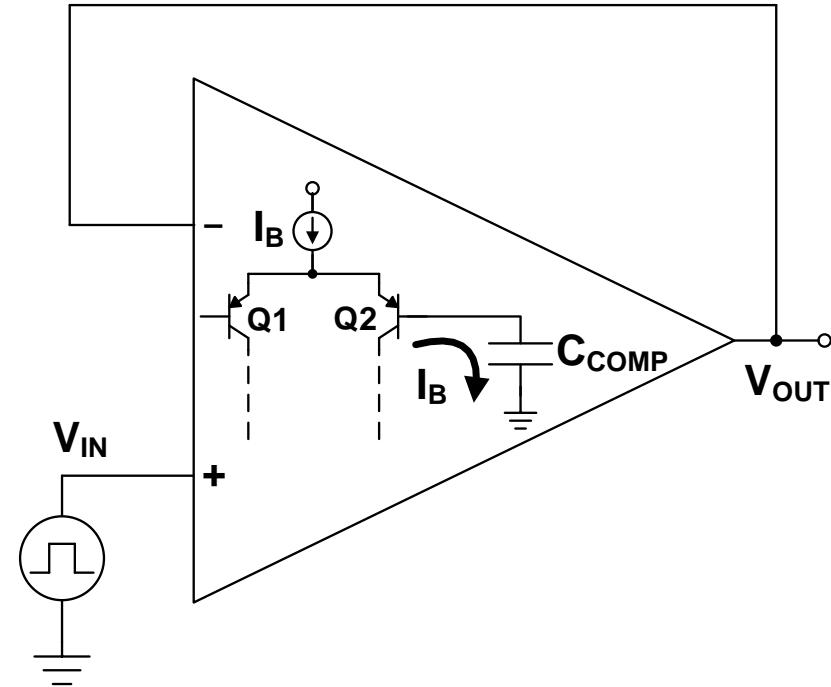


$$I_N = I_1 - I_2$$

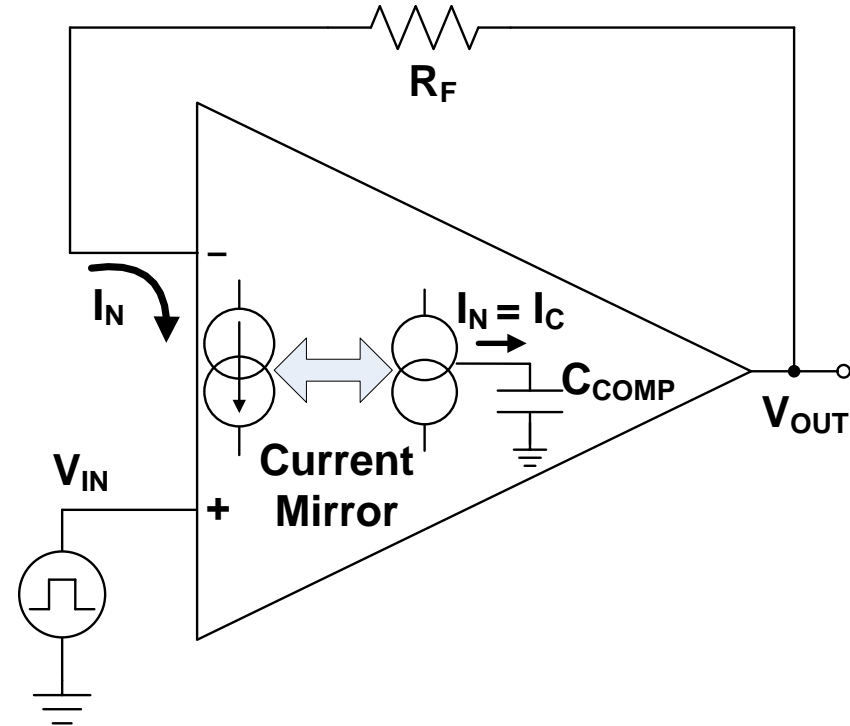
$$I_N = I_C$$

# Slew Rate VFB vs CFB

## VFB



## CFB



# Slew Rate: VFB vs CFB

## Current Feedback

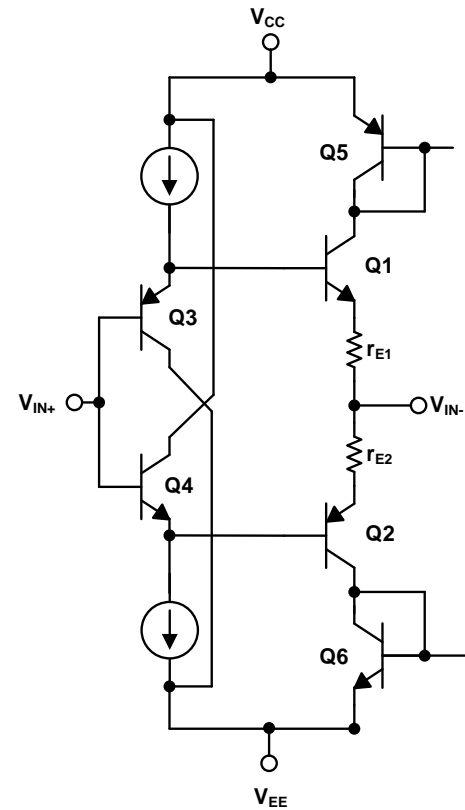
Device	Slew Rate (V/ $\mu$ s)	$I_Q$ (mA)
OPA683	210	0.79
OPA684	820	1.7
OPA691	2100	5.1
OPA695	4300	12.9
<b>THS3001</b>	<b>6300</b>	<b>6.6</b>
<b>THS3061</b>	<b>7000</b>	<b>8.3</b>
<b>THS3091</b>	<b>7300</b>	<b>9.5</b>

## Voltage Feedback

Device	Slew Rate (V/ $\mu$ s)	$I_Q$ (mA)
THS4281	35	0.8
LMH6619	57	1.45
OPA820	240	5.6
OPA846	625	12.6
<b>OPA637</b>	<b>100</b>	<b>7</b>
<b>THS4051</b>	<b>240</b>	<b>8.5</b>
<b>THS4631</b>	<b>1000</b>	<b>11.5</b>

Products in bold text are high-voltage op-amps with max. supply >24V

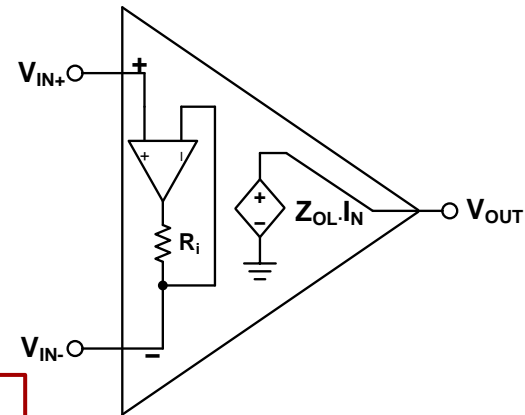
# Low-Power CFB Amplifier Designs



$$r_E = \frac{V_T}{I_E}$$

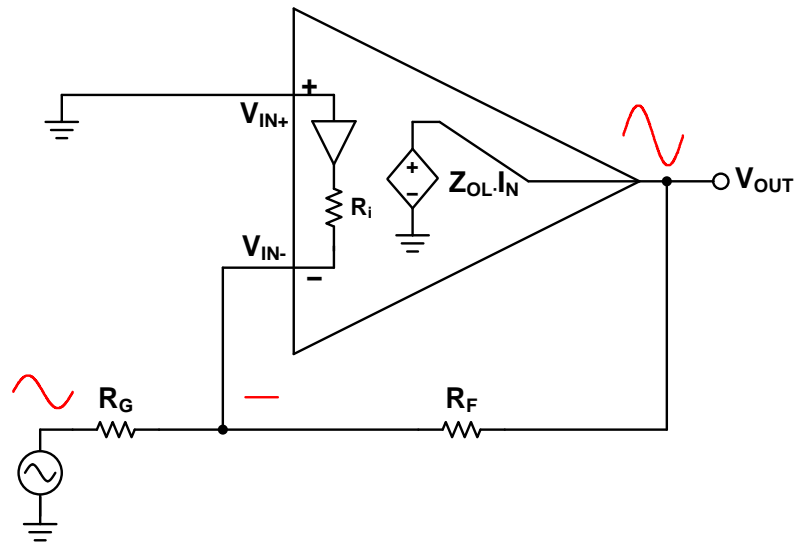
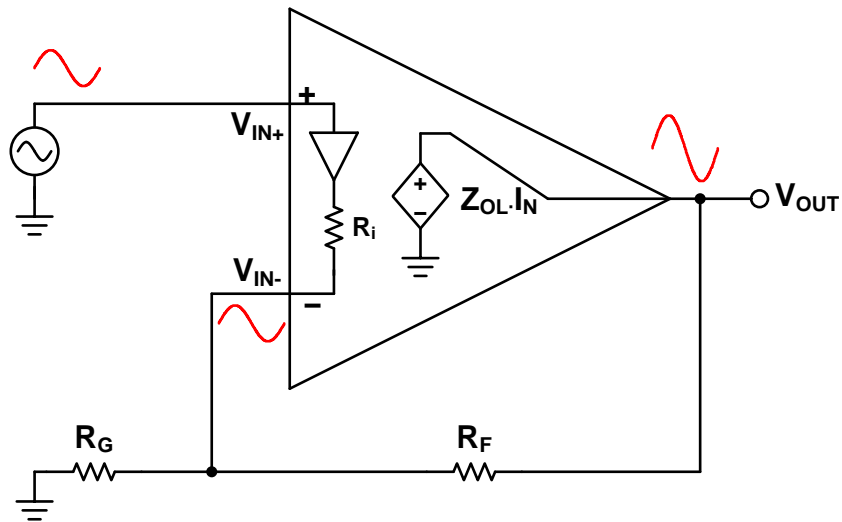
$r_E$  = Emitter Resistance  
 $V_T$  = Thermal Voltage  
 $I_E$  = Emitter Current

$$\text{Feedback Transimpedance} = (R_F + R_i \times \text{NoiseGain})$$



Specification	OPA691 (Open Loop Buffer)	OPA683 (Closed Loop Buffer)
Quiescent Current, $I_Q$	5.1 mA	0.82 mA
Inverting Input Resistance, $R_i$	35 $\Omega$	4.5 $\Omega$

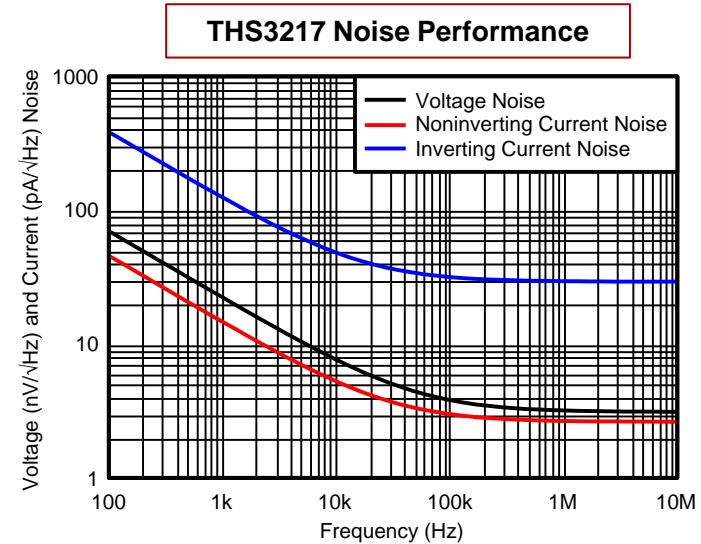
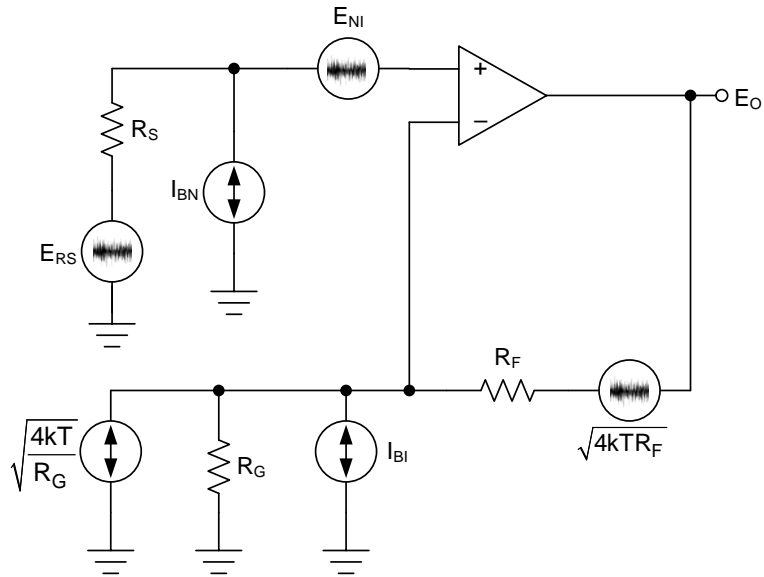
# Noninverting versus Inverting Configuration



Slew rate (25% to 75% level)	$G = 2, V_O = 10\text{-V step}, R_F = 1.21\text{ k}\Omega$	$T_A = 25^\circ\text{C}$	5000	V/ $\mu\text{s}$
	$G = 5, V_O = 20\text{-V step}, R_F = 1\text{ k}\Omega$	$T_A = 25^\circ\text{C}$	7300	

$$\text{Slew Rate} = 8V_{\text{PEAK}} \cdot 2\pi \cdot 100\text{MHz} = 5025\text{V} / \mu\text{sec}$$

# CFB Noise Analysis



$E_{NI}$  = Amplifier Voltage Noise

$i_{BN}$  = Noninverting Current Noise

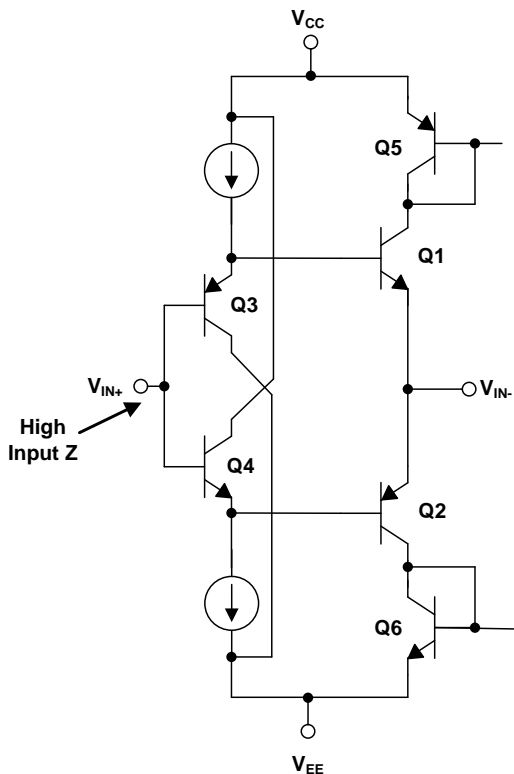
$i_{BI}$  = Inverting Current Noise

$G_N$  = Noise Gain =  $(1 + R_F/R_G)$

$$E_0 = \sqrt{(E_{NI}^2 + (i_{BN}R_S)^2 + 4kTR_S)G_N^2 + (i_{BI}R_F)^2 + 4kTR_FG_N}$$



# Input Bias Current and Current Noise



Specification	THS4271 (VFA)	OPA695 (CFA)	Units
$I_B$ , Non-inverting Bias Current	6	$\pm 13$	$\mu A$
$I_B$ , Inverting Bias Current		$\pm 20$	$\mu A$
$I_{BOS}$ , Bias Current Offset	$\pm 1$	20	$\mu A$
Non-inverting Bias Current Noise	3	18	$pA/\sqrt{Hz}$
Inverting Bias Current Noise		22	$pA/\sqrt{Hz}$

# Summary Comparison

Parameters	VFA	CFA
DC Accuracy	<b>Good</b>	Poor
Output Swing	<b>Many rail-to-rail output options</b>	Larger headroom needed for output
Distortion	Better low-frequency distortion	Better high-frequency distortion
Slew Rate	Limited slew rate	<b>Very high slew rate facilitating high full-power bandwidth</b>
Bandwidth	Bandwidth varies with gain	<b>Almost constant bandwidth over gain</b>
Gain Stability	Restriction on the minimum stable gain for decompensated amplifiers	<b>Stable across gains if feedback transimpedance is kept constant</b>
Noise	<b>Low input-referred voltage and current noise</b>	Higher input-referred current noise (unequal for inverting and non-inverting inputs)
Typical Applications	<ul style="list-style-type: none"><li>- Applications requiring DC precision</li><li>- Pulse-oriented application</li><li>- High-speed and precise ADC interface</li><li>- Transimpedance</li></ul>	<ul style="list-style-type: none"><li>- DAC interface</li><li>- Output drivers</li><li>- High-speed ADC interface</li><li>- Sallen-Key filters.</li></ul>



Thanks for your time and please  
take the quiz!