

Non-isolated Current Sensing in Low Voltage Battery Management System (BMS)

Key Considerations

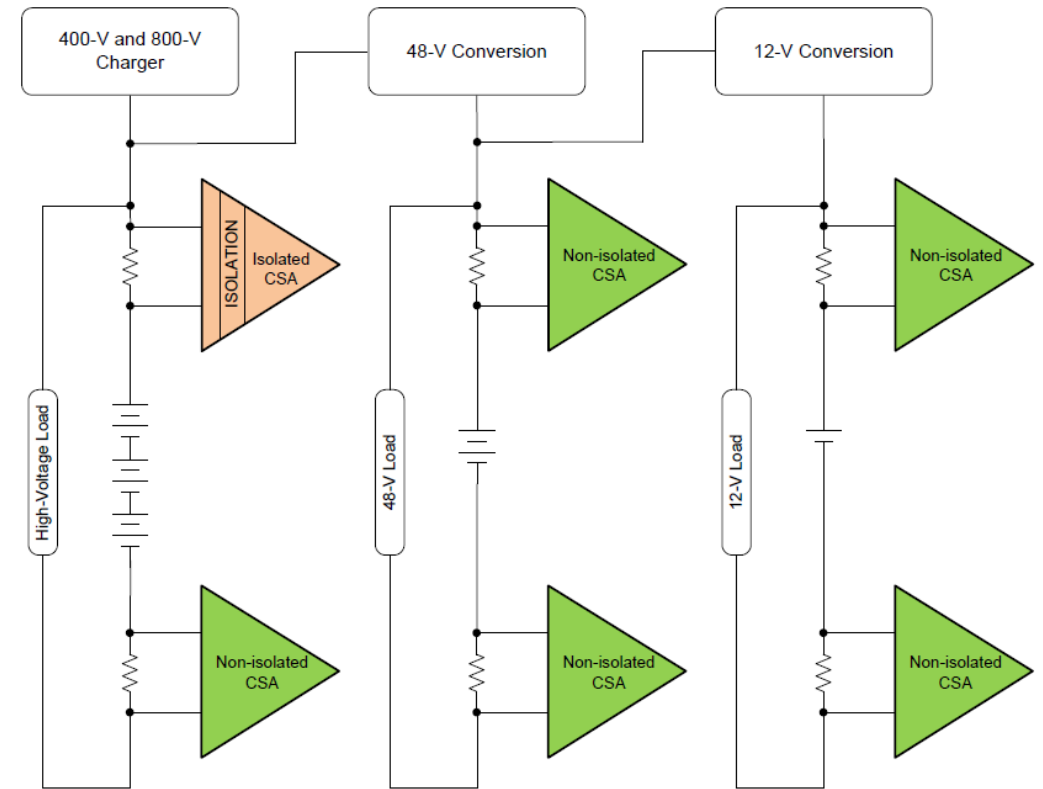
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Topics

- Current sensing configuration in BMS
- Nonisolated shunt based current sensing in BMS and charging system
- How to size the shunt resistor
- Key specification of the CSA and how to choose the right CSA

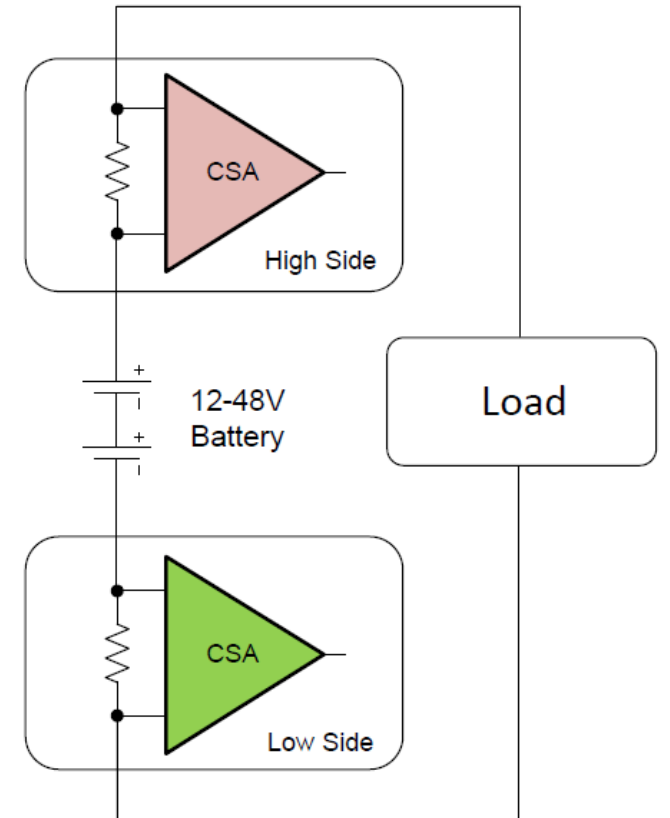
Overview of shunt based current sensing in EV BMS – Location Matters!

- Top of stack
 - High voltage battery system –
 - Isolated current sensing device, including magnetic.
 - Floating supply - With the help of special circuit techniques and isolation devices, a low voltage CSA can sometimes be adapted for high voltage applications see the next couple of slides
 - Low voltage battery system –
 - 12V to 48V
 - Possible to use CSA directly
- Bottom of stack
 - The common mode voltage requirement is less stringent
 - Much wider selection of CSA
- Challenges of current sensing BMS
 - Wide current range
 - Accuracy requirement at both the high and low end of the current range.



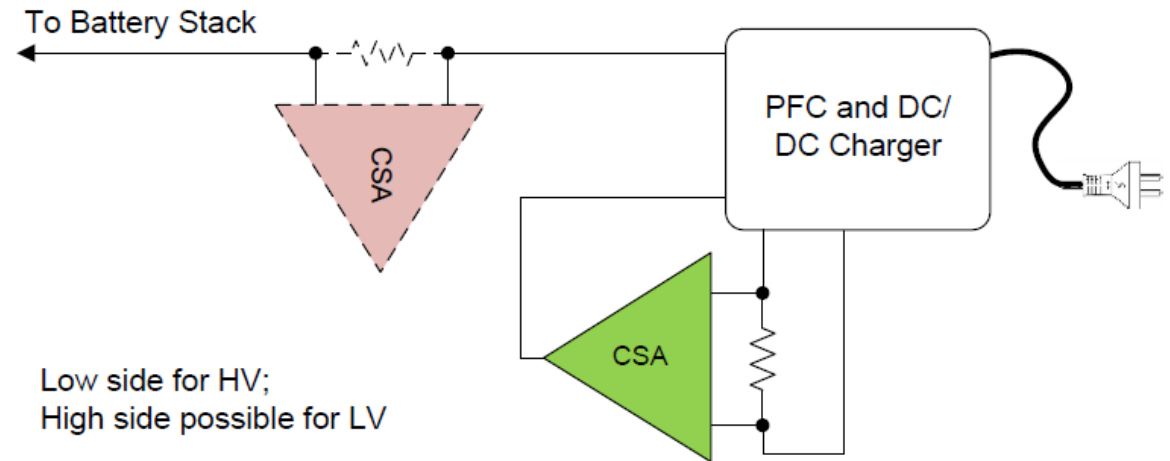
Non-Isolated CSA for BMS

- Compared to isolated CSA, non-isolated CSA has the following advantages
 - Simple to implement
 - low cost
 - excellent linearity,
 - Accuracy
- However it has the following drawbacks
 - Invasive
 - Shunt resistor dissipates power in the form of heat
 - Common mode input range may limit CSM to low side configuration



Non-Isolated CSA in Vehicle Charger

- Types of battery technology
 - Li-Ion
 - Lead acid
 - Other Less common but actively researched
- Why is current sensing required in chargers
 - Maintain a specific charging profile
 - Safety
- Challenges
 - Large current range
 - Common mode voltage




How to size the shunt resistor for BMS application

- Shunt resistor is determined by:
 - Upper bound – power dissipation
 - Lower bound – minimum detectable current
- An example
 - Max current 100A; min current 1A
 - With max $R_{shunt}=1\text{m}\Omega$, $P = I^2R = (100\text{A})^2 \times 1\text{m}\Omega = 10\text{W}$!
 - What about $100\mu\Omega$ shunt? $P = I^2R = (100\text{A})^2 \times 100\mu\Omega = 1\text{W}$
 - At lowest current, $V_{sense} = IR = (1\text{A}) \times 100\mu\Omega = 100\mu\text{V}$
- The final R_{shunt} also depends on the accuracy requirement and which CSA to choose
 - If $V_{os} = \pm 100\mu\text{V}$, effective total input to the ideal CSA is $V_{in} = 100\mu\text{V} \pm 100\mu\text{V} = 0\mu\text{V to } 200\mu\text{V}$. Then $100\mu\Omega$ is probably too small
 - If $V_{os} = \pm 10\mu\text{V}$, then the effective total input to the ideal CSA is $V_{in} = 100\mu\text{V} \pm 10\mu\text{V} = 90\mu\text{V to } 110\mu\text{V}$.

Current Sensing Key Considerations

- **Configuration**
 - High side; Low side
- **Directionality**
 - Uni-directional swing; Bi-directional swing
- **Output**
 - Analog (voltage/current); Digital
 - Integrated shunt
- **Speed**
 - System bandwidth
- **DC error sources**
 - Vos; Gain error; CMRR; PSRR; IB;
- **Noise**
- **Temperature drift**

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INA240
SBOS662B – JULY 2016 – REVISED FEBRUARY 2018

INA240 High- and Low-Side, Bidirectional, Zero-Drift, Current-Sense Amplifier With Enhanced PWM Rejection

1 Features

- Enhanced PWM Rejection
- Excellent CMRR:
 - 132-dB DC CMRR
 - 93-dB AC CMRR at 50 kHz
- Wide Common-Mode Range: –4 V to 80 V
- Accuracy:
 - Gain:
 - Gain Error: 0.20% (Maximum)
 - Gain Drift: 2.5 ppm/°C (Maximum)
 - Offset:
 - Offset Voltage: ±25 µV (Maximum)
 - Offset Drift: 250 nV/°C (Maximum)
- Available Gains:
 - INA240A1: 20 V/V
 - INA240A2: 50 V/V
 - INA240A3: 100 V/V
 - INA240A4: 200 V/V
- Quiescent Current: 2.4 mA (Maximum)

2 Applications

- Motor Controls
- Solenoid and Valve Controls
- Power Management
- Actuator Controls
- Pressure Regulators
- Telecom Equipment

3 Description

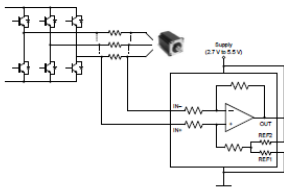
The INA240 device is a voltage-output, current-sense amplifier with enhanced PWM rejection that can sense drops across shunt resistors over a wide common-mode voltage range from –4 V to 80 V, independent of the supply voltage. The negative common-mode voltage allows the device to operate below ground, accommodating the flyback period of typical solenoid applications. Enhanced PWM rejection provides high levels of suppression for large common-mode transients ($\Delta V/\Delta t$) in systems that use pulse width modulation (PWM) signals (such as motor drives and solenoid control systems). This feature allows for accurate current measurements without large transients and associated recovery ripple on the output voltage.

This device operates from a single 2.7-V to 5.5-V power supply, drawing a maximum of 2.4 mA of supply current. Four fixed gains are available: 20 V/V, 50 V/V, 100 V/V, and 200 V/V. The low offset of the zero-drift architecture enables current sensing with maximum drops across the shunt as low as 10-mV full-scale. All versions are specified over the extended operating temperature range (–40°C to +125°C), and are offered in an 8-pin TSSOP and 8-pin SOIC packages.

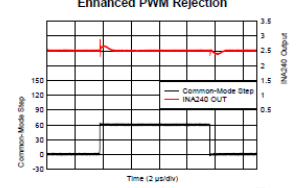
Device Information(1)		
PART NUMBER	PACKAGE	BODY SIZE (NOM)
INA240	TSSOP (8)	3.00 mm × 4.40 mm
	SOIC (8)	4.00 mm × 3.91 mm


(1) For all available packages, see the orderable addendum at the end of the data sheet.


Typical Application



Enhanced PWM Rejection



 An IMPORTANT NOTICE at the end of this data sheet addresses availability, warranty, changes, use in safety-critical applications, intellectual property matters and other important disclaimers. PRODUCTION DATA.


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7.5 Electrical Characteristics

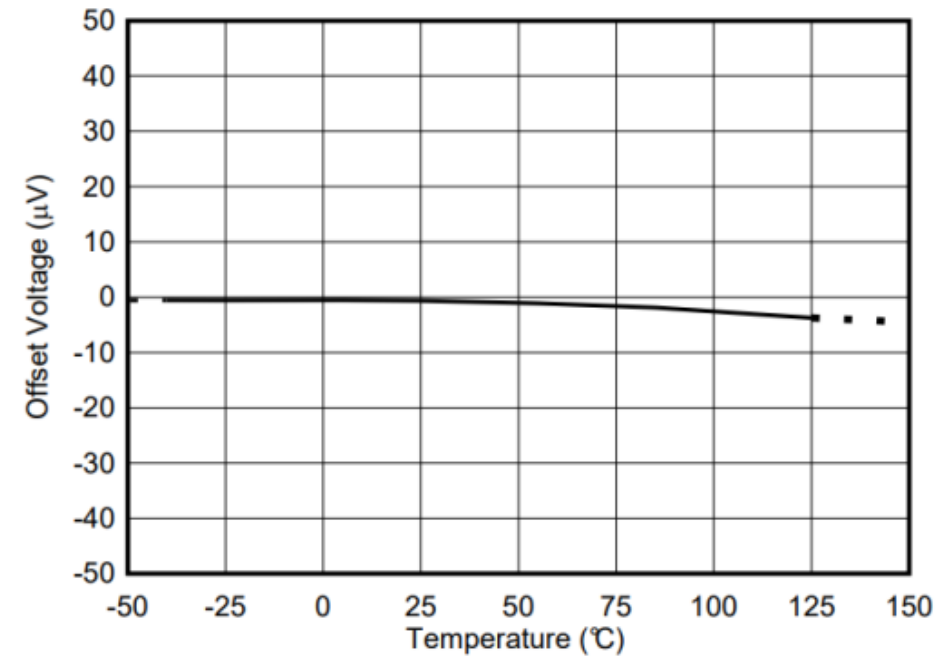
at $T_A = 25^\circ\text{C}$, $V_S = 5\text{ V}$, $V_{CM(EN)} = V_{IN-} = V_{IN+}$, $V_{OUT} = 12\text{ V}$, and $V_{REF1} = V_{REF2} = V_{REF} / 2$ (unless otherwise noted)

INPUT	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
V _{CM}	Common-mode input range	$V_{IN-} = -4\text{ V to } 80\text{ V}$, $V_{IN+} = 0\text{ mV}$ $T_A = -40^\circ\text{C to } 125^\circ\text{C}$	–4		80	V
		$V_{IN-} = -4\text{ V to } 80\text{ V}$, $V_{IN+} = 0\text{ mV}$ $T_A = -40^\circ\text{C to } 125^\circ\text{C}$	120	132		
CMRR	Common-mode rejection ratio	$V_{IN-} = -4\text{ V to } 80\text{ V}$, $V_{IN+} = 0\text{ mV}$ $T_A = -40^\circ\text{C to } 125^\circ\text{C}$		93		dB
		$f = 50\text{ kHz}$		±25		µV
V _{OS}	Offset voltage, input-referred	$V_{IN+} = 0\text{ mV}$, $T_A = -40^\circ\text{C to } 125^\circ\text{C}$	±50	±250		mV/°C
dV_{OS}/dT	Offset voltage drift	$V_{IN+} = 0\text{ mV}$, $T_A = -40^\circ\text{C to } 125^\circ\text{C}$	±50	±250		mV/°C
PSRR	Power-supply rejection ratio	$V_{IN} = 2.7\text{ V to } 5.5\text{ V}$, $V_{IN+} = 0\text{ mV}$ $T_A = -40^\circ\text{C to } 125^\circ\text{C}$	±1	±10		µV/V
I _b	Input bias current	I_{IN-} , I_{IN+} , $V_{IN+} = 0\text{ mV}$		90		µA
		Reference input range		0	V_{REF}	V
OUTPUT						
G	gain	INA240A1		20		V/V
		INA240A2		50		
		INA240A3		100		
		INA240A4		200		
Gain error	$GND + 50\text{ mV} = V_{OUT} = V_{REF} - 200\text{ mV}$ $T_A = -40^\circ\text{C to } 125^\circ\text{C}$		±0.05%	±0.20%		
		$GND + 10\text{ mV} = V_{OUT} = V_{REF} - 200\text{ mV}$		±0.01%		
Non-linearity error	$GND + 10\text{ mV} = V_{OUT} = V_{REF} - 200\text{ mV}$		±0.01%			
		Reference divider accuracy	$V_{REF1} = V_{REF2} - V_{REF} / 2$ at $V_{IN+} = 0\text{ mV}$, $T_A = -40^\circ\text{C to } 125^\circ\text{C}$		0.02%	0.1%
RVRR	Reference voltage rejection ratio (input-referred)	INA240A1		20		µV/V
		INA240A3		5		
		INA240A2, INA240A4		2		
	Maximum capacitive load	No sustained oscillation	1			nF
VOLTAGE OUTPUT(1)						
Swing to V_S power-supply rail	$R_L = 10\text{ k}\Omega$ to GND $T_A = -40^\circ\text{C to } 125^\circ\text{C}$		$V_{REF} - 0.05$	$V_{REF} - 0.2$		V
		Swing to GND	$R_L = 10\text{ k}\Omega$ to GND, $V_{IN+} = 0\text{ mV}$ $V_{REF1} = V_{REF2} = 0\text{ V}$, $T_A = -40^\circ\text{C to } 125^\circ\text{C}$	$V_{REF} + 1$	$V_{REF} + 10$	
FREQUENCY RESPONSE						
BW	Bandwidth	All gains, –3-dB bandwidth		400		kHz
		All gains, 2% THD+N(2)		100		
		Settling time - output settles to 0.5% of final value		9.6		
SR	Slew rate	INA240A1		9.8		V/µs
		INA240A4		2		
NOISE (INPUT REFERRED)						
	Voltage noise density			40		mV/√Hz
POWER SUPPLY						
V _S	Operating voltage range	$T_A = -40^\circ\text{C to } 125^\circ\text{C}$	2.7	5.5		V
I _Q	Quiescent current	$V_{IN+} = 0\text{ mV}$		1.8	2.4	mA
		I_{IN-} vs temperature, $T_A = -40^\circ\text{C to } 125^\circ\text{C}$			2.6	
TEMPERATURE RANGE						
	Specified range		–40	125		°C

(1) See Figure 13.
(2) See the **Input Signal Bandwidth** section for more details.

CSA Specification – Temperature Drift Example

- The best
 - Room temp Vos 25uV; Drift: 250nV/°C;
- At 105°C
 - $V_{os} \leq 25 + 0.25 * 80 = 45\mu V$
- A good, but not the best:
 - Identical room temp spec; Drift: 1uV/°C
 - $V_{os} \leq 25 + 1 * 80 = 105\mu V$



For more info www.ti.com/currentsense